

Ground Bearing Pressure: Practical Applications for Lifts of All Sizes



Host:

Mike Parnell
President/CEO,
Industrial Training International



Guest Speaker:

Jim Jatho
Heavy Lift & Rigging Planner,
Buckner Heavylift Cranes

The views expressed in this presentation are that of ITI and are not necessarily the views of the ASME or any of its committees



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- Crane Accident Investigation
- Terex Presents: Ground Condition and Preparation for Mobile Cranes
- Rigger & Signal Person 1926.1400
- Ground Condition Surveys & Stabilization Techniques
- Winch, Drag or Roll?

Today's Presentation:

Ground Bearing Pressure: Practical Applications for Lifts of All Sizes

Coming up Next:

Load Distribution: Trolley Beams and 2-Crane Picks

MIKE PARNELL— ABOUT YOUR HOST

Mr. Parnell has a wealth of knowledge regarding cranes, rigging, and lifting activities throughout a variety of industries.

- 30+ years learning about wire rope, rigging, load handling, and lifting activities.
- Vice Chair of the ASME B30 Main Committee which sets the standards in the U.S. for cranes and rigging.
- Chair of the AMSE P30 Main Committee which sets the standards for lift planning.

ASME standards are also adopted by many countries around the world.



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JIM JATHO – ABOUT YOUR GUEST SPEAKER

Mr. Jatho is still a newcomer to the heavy lift industry with only three years experience, but in that time has achieved 100+ Critical Lifts planned and executed without incident:

- In environments including oil refineries, chemical plants, fertilizer plants, windfarms, and nuclear power plants
- Involving cranes as large as 750 tonnes in capacity, and currently developing preliminary plans for the new Liebherr 1000 tonne crane.
- All while developing his own tools and software to aid in the lift planning process



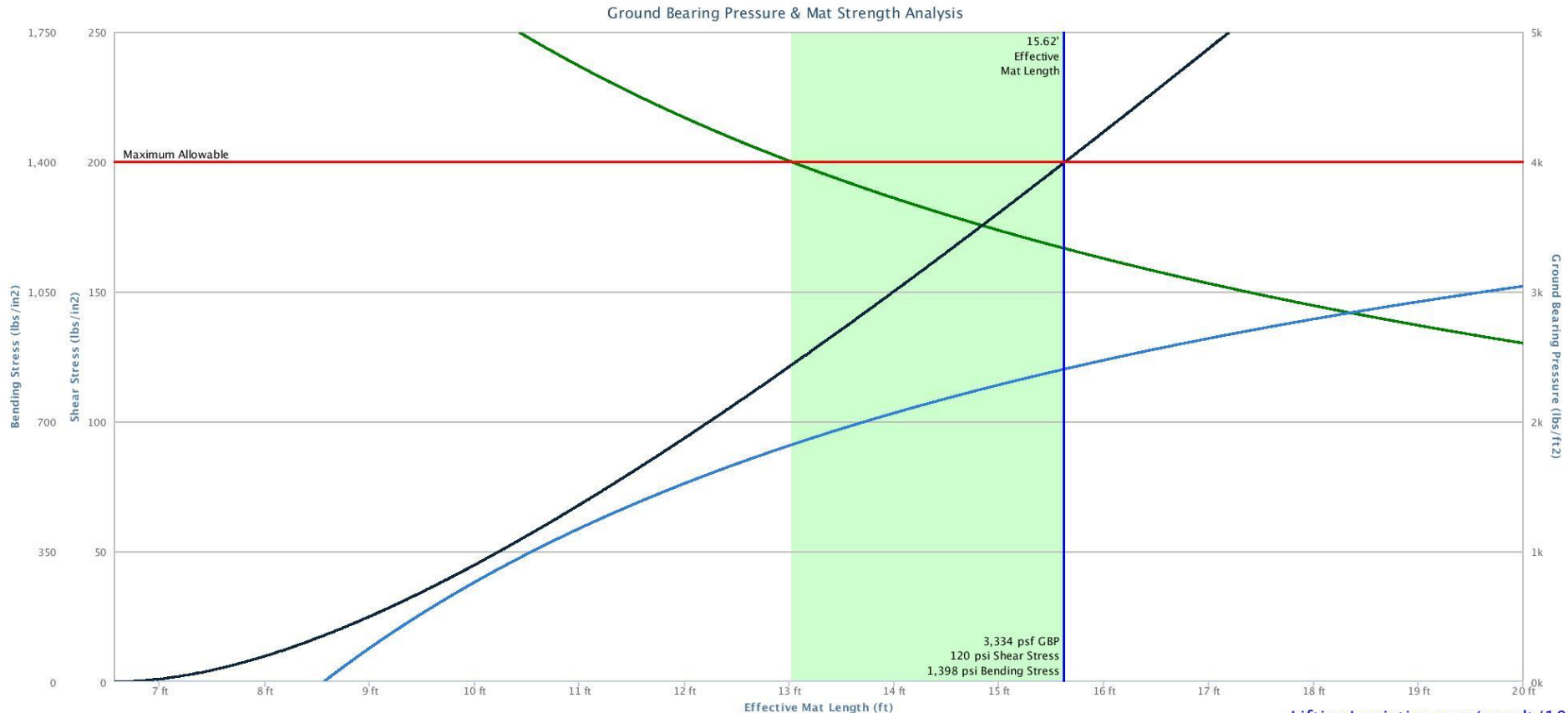
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BUCKNER
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STEEL / PRECAST / STACK ERECTION
HEAVYLIFT CRANES
INDUSTRIAL RIGGING
MISCELLANEOUS FABRICATION

Ground Bearing Pressure: Practical Applications for Lifts of All Sizes

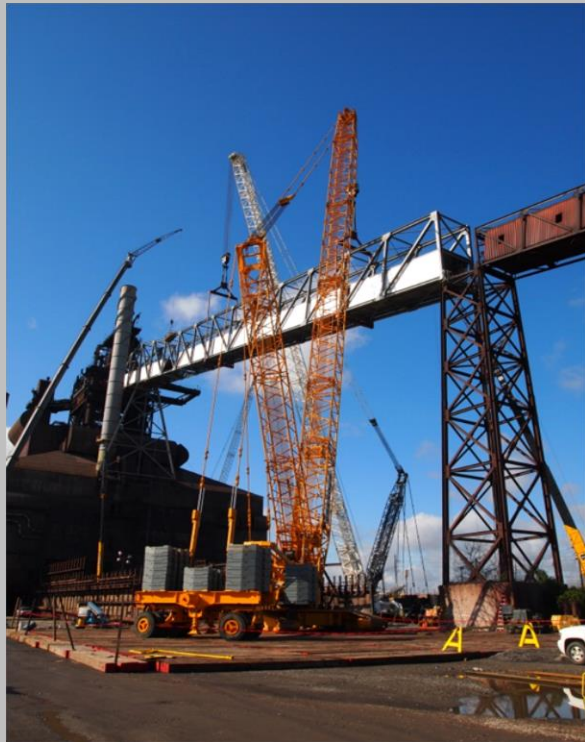




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HEAVYLIFT CRANES
INDUSTRIAL RIGGING
MISCELLANEOUS FABRICATION**

going the distance...since 1947



Rankings

National Ranking

American Crane and Transport

#13-most cranes (Total Lift Capacity)

#7- largest crane

#8-largest crawler crane fleet



Engineering News Record

#9-Steel Erection

World Ranking

International Crane

#22- most cranes (Total Lift Capacity)



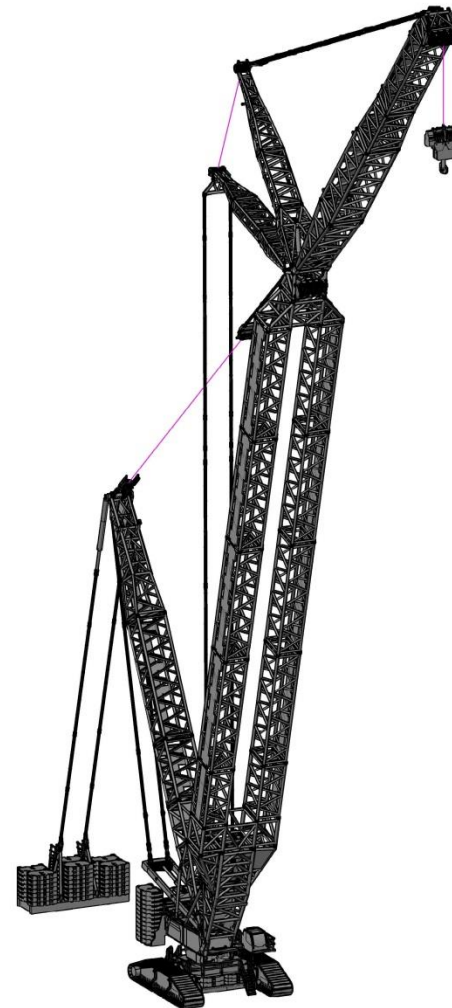
Our Fleet

CRAWLER CRANE FLEET

multiple units

| | |
|--------------------------------|---------|
| IHI CCH-700 | 72T |
| Terex HC-80 | 80T |
| Mantis Tele-Crawler 20010 | 100T |
| Liebherr Tele-Crawler LTR-1100 | 110T |
| Terex HC-110 | 110T |
| Kobelco CK-1600 | 160T |
| Manitowoc 777 | 200T |
| Manitowoc 888 | 230T |
| Manitowoc 999 | 275T |
| Liebherr LR-1350 | 385T |
| Liebherr LR-1400/1&2 | 440T** |
| Demag 2800-1/NT | 660T** |
| Liebherr LR-1600/2 | 660T** |
| Liebherr LR-1750 | 825T** |
| Liebherr LR-11000 | 1100T** |
| Liebherr LR-11000/P1300 | 1433T** |

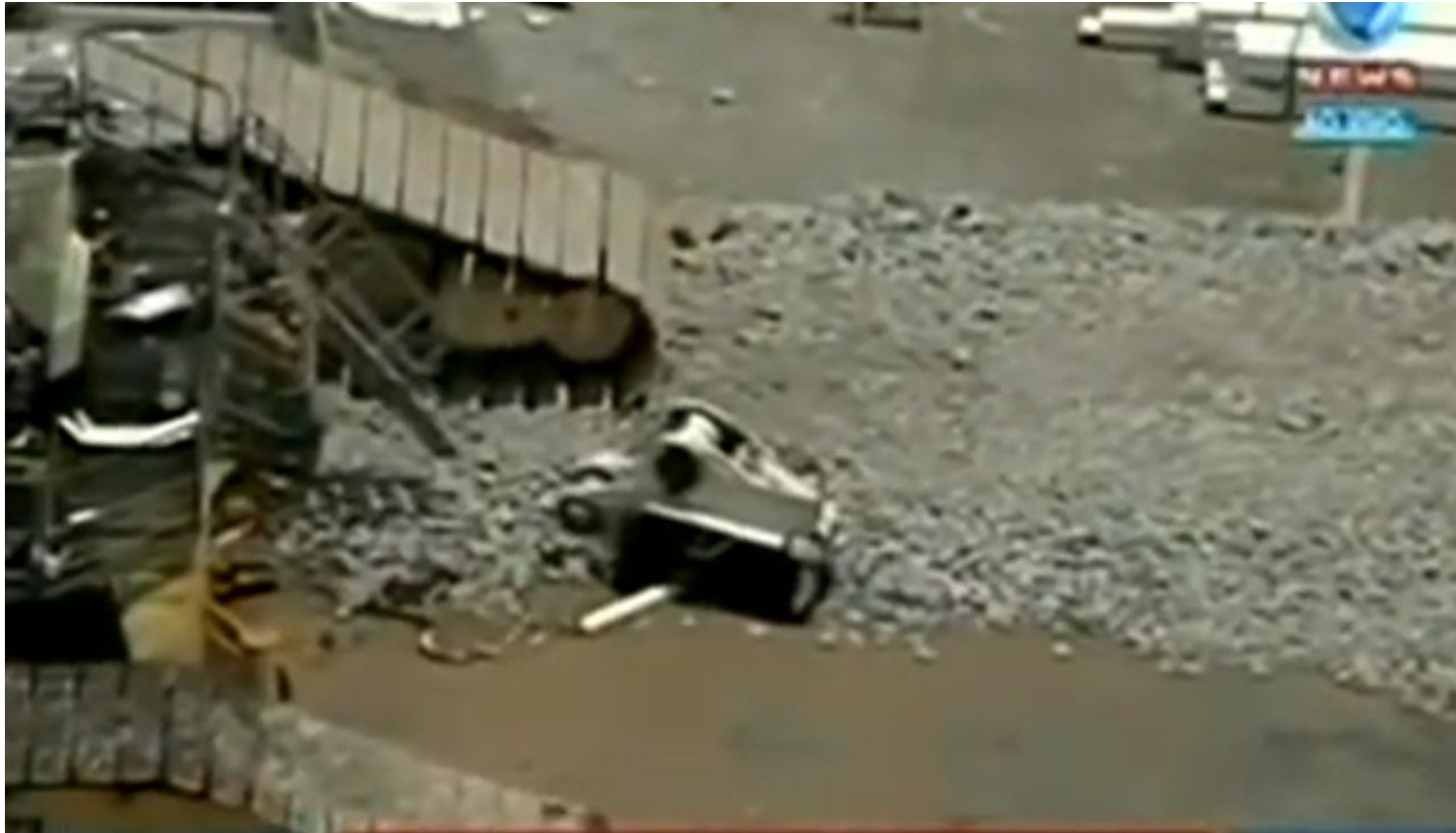
**Significant capacity increase
when utilizing heavy lift attachments



The Reason



The Reason



The Data



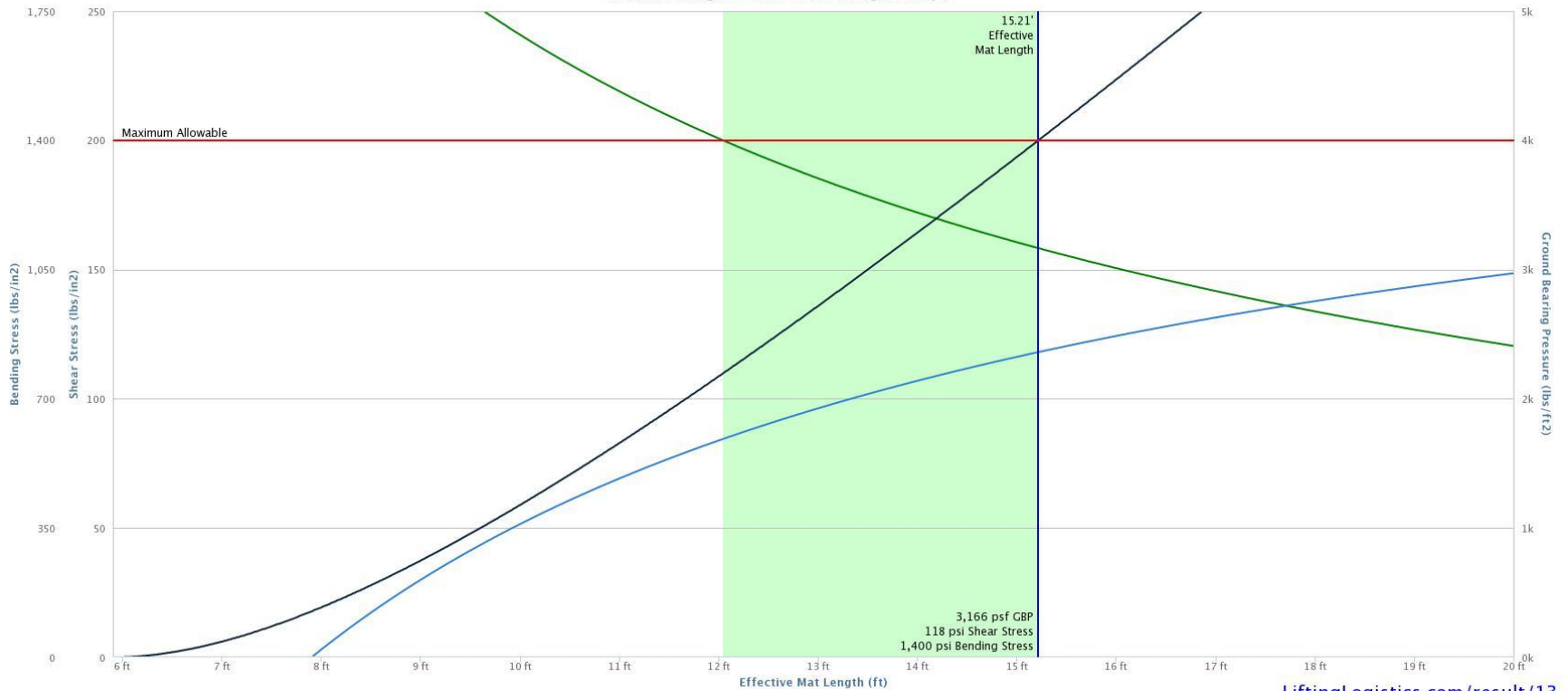
*- LR 11350, 102m Main Boom,
42m Derrick with Ballast Tray*

*- 2,185 tonnes gross crane
weight*

*- 39.02 tonnes / m²
(7,993lbs/ft²) Beneath tracks*

*- “The LR11350 was only
working at 82% of the Load
Chart”*

Ground Bearing Pressure & Mat Strength Analysis

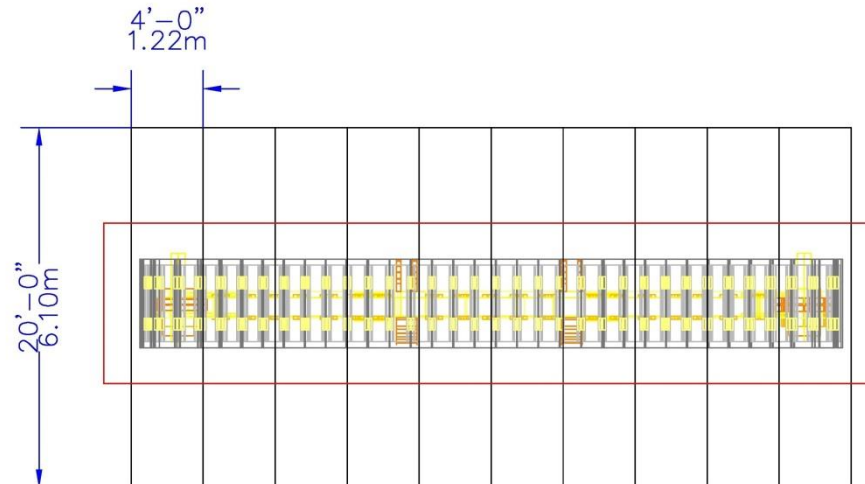
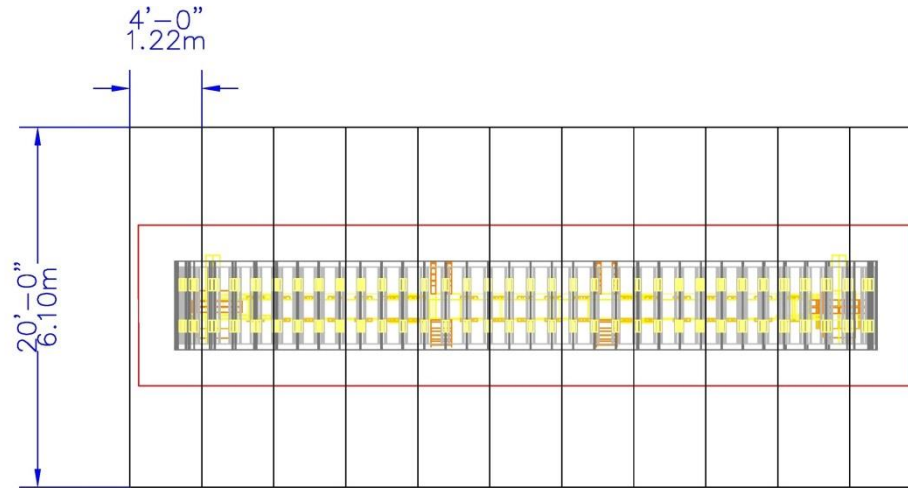


LiftingLogistics.com/result/13

| | | | | | | |
|------------------------------------|---------------------------|--------------------------------------|---------------------------|----------------------------------|---------------------------|------------------------------|
| T_L Track bearing length | 37.00 ft | Soil Bearing Method | | Mat Strength Method | | Ground bearing pressure: |
| C Bearing width of track | 5.90 ft | P Load applied to one mat | 188,635 lbs | p Crane load applied to one mat | 188,635 lbs | 79.16% of allowable capacity |
| T_{TL} Track toe load | 7,993 lbs/ft ² | A_{reqd} Required mat bearing area | 48.16 ft ² | L_c Cantilevered length of mat | 4.66 ft | Bending stress in mat: |
| T_{HL} Track heel load | 7,993 lbs/ft ² | L_{reqd} Required effective length | 12.04 ft | q GBP due to P | 3,101 lbs/ft ² | 99.98% of allowable capacity |
| B Mat width | 4.0 ft | L_c Cantilevered length of mat | 3.07 ft | M Bending moment in the mat | 1,612,439 lb-in | Shear stress in mat: |
| W Mat Length | 20.0 ft | q GBP due to P | 3,917 lbs/ft ² | f_b Bending stress due to M | 1400 lbs/in ² | 59.02% of allowable capacity |
| d Mat thickness | 12.0 in | M Bending moment in the mat | 885,909 lb-in | V Shear in the mat | 45,329 lbs | |
| W Weight of mat | 4,000 lbs | f_b Bending stress due to M | 769 lbs/in ² | f_v Shear stress due to V | 118 lbs/in ² | |
| q_a Allowable GBP | 4,000 lbs/ft ² | V Shear in the mat | 32,430 lbs | q_t actual GBP | 3,166 lbs/ft ² | |
| F_b Allowable bending stress | 1,400 lbs/in ² | f_v Shear stress due to V | 84 lbs/in ² | | | |
| F_v Allowable shear stress | 200 lbs/in ² | q_t Maximum GBP | 4,000 lbs/ft ² | | | |
| L_{eff} Assumed effective length | 15.21 ft | | | | | |

Pressure Beneath Mats: 3,166lbs/ft²

Where This Started



The Source

- Mat Length Based on Soil Bearing Capacity
- Mat Length Based on Mat Strength



Effective Bearing Length of Crane Mats

David Duerr, P.E.
2DM Associates, Inc., Consulting Engineers
Houston, Texas

INTRODUCTION

Crane mats are used to distribute the high concentrated loads from mobile cranes over a relatively large ground area so that the soil is loaded at tolerable bearing pressures. This has been common construction industry practice for many decades. Although crane mats are most commonly made of heavy timbers, fabricated steel mats are occasionally used under large cranes or when soil conditions are poor.

The analysis of a crane mat requires a determination of the length of the mat that actually bears on the soil and contributes to the support of the crane. At working loads, this is a relatively simple "beam on an elastic foundation" problem. However, such a solution may not produce a realistic result due to the nonlinearity of the soil as the ultimate bearing capacity is approached. Further, the elastic properties of the soil needed to perform such an analysis are not often available.

The purpose of this paper is to develop a practical means of calculating the effective bearing length of a crane mat that is based on readily available values and that produces an acceptably safe and reliable result.

CURRENT PRACTICE

Engineers in construction presently use a number of different approaches to design crane mats. The two most common of these methods are described here.

Mat Length Based on Soil Bearing Capacity

This crane mat design method is the most straightforward. Once the load from the crane has been calculated, whether an outrigger load or a crawler track pressure, the required crane mat area is calculated by dividing the crane load plus the weight of the mat by the allowable ground bearing pressure. Divide this area by the width of the mat and we have the required effective bearing length. This mat length is then used to calculate bending and shear stresses in the mat, based on the assumption of a uniform pressure equal to the crane load divided by the bearing area acting upward on the bottom of the mat. If the actual stresses are equal to or less than the allowable stresses, the mat is acceptable. This method can be

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written in equation form as follows. The basic arrangement is illustrated in Fig. 1. Note that Eqs. 7 and 8 are written for the design of timber crane mats. The term d in Eq. 7 and the coefficient 1.5 in Eq. 8 are not used for the design of steel mats.

$$A_{reqd} = \frac{P + W}{q_a} \quad (1)$$

$$L_{reqd} = \frac{A_{reqd}}{B} \quad (2)$$

$$L_c = \frac{L_{reqd} - C}{2} \quad (3)$$

$$q = \frac{P}{L_{reqd} B} \quad (4)$$

$$M = \frac{(qB) L_c^2}{2} \quad (5)$$

$$f_b = \frac{M}{Bd^2/6} \leq F_b \quad (6)$$

$$V = (qB)(L_c - d) \quad (7)$$

$$f_v = \frac{1.5V}{Bd} \leq F_v \quad (8)$$

where:

P = crane load applied to one mat,
 W = self-weight of the mat;

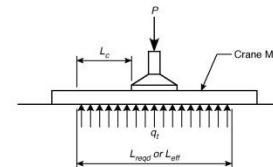


Fig. 1. Simple Crane Mat Arrangement

Presented at the Crane & Rigging Conference
Houston, Texas May 26 - 27, 2010

Mat Length Based on Soil Bearing Capacity

$$A_{reqd} = \frac{P + W}{q_a} \quad (1)$$

$$L_{reqd} = \frac{A_{reqd}}{B} \quad (2)$$

$$L_c = \frac{L_{reqd} - C}{2} \quad (3)$$

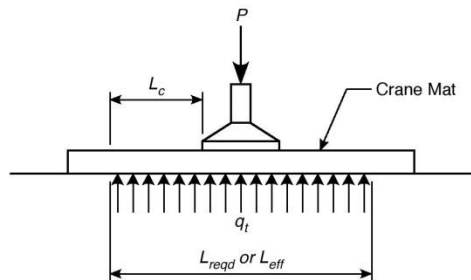
$$q = \frac{P}{L_{reqd}B} \quad (4)$$

$$M = \frac{(qB)L_c^2}{2} \quad (5)$$

$$f_b = \frac{M}{Bd^2/6} \leq F_b \quad (6)$$

$$V = (qB)(L_c - d) \quad (7)$$

$$f_v = \frac{1.5V}{Bd} \leq F_v \quad (8)$$



- P = crane load applied to one mat;
- W = self-weight of the mat;
- q_a = allowable ground bearing pressure;
- A_{reqd} = required mat bearing area;
- B = mat width;
- L_{reqd} = required effective bearing length of the mat;
- C = bearing width of the track or outrigger pad;
- L_c = cantilevered length of the mat;
- q = ground bearing pressure due to P ;
- M = bending moment in the mat;
- d = mat depth (or thickness);
- f_b = bending stress due to M ;
- F_b = allowable bending stress;
- V = shear in the mat;
- f_v = shear stress due to V ; and,
- F_v = allowable shear stress.

Mat Length Based on Mat Strength

$$L_c = \frac{L_{eff} - C}{2} \quad (9)$$

$$q = \frac{P}{L_{eff}B} \quad (10)$$

$$M = \frac{(qB)L_c^2}{2} \quad (11)$$

$$f_b = \frac{M}{Bd^2/6} = F_b \quad (12)$$

$$V = (qB)(L_c - d) \quad (13)$$

$$f_v = \frac{1.5V}{Bd} = F_v \quad (14)$$

$$q_t = \frac{P + W}{L_{eff}B} \leq q_a \quad (15)$$

- P = crane load applied to one mat;
- W = self-weight of the mat;
- q_a = allowable ground bearing pressure;
- A_{reqd} = required mat bearing area;
- B = mat width;
- L_{reqd} = required effective bearing length of the mat;
- C = bearing width of the track or outrigger pad;
- L_c = cantilevered length of the mat;
- q = ground bearing pressure due to P ;
- M = bending moment in the mat;
- d = mat depth (or thickness);
- f_b = bending stress due to M ;
- F_b = allowable bending stress;
- V = shear in the mat;
- f_v = shear stress due to V ; and,
- F_v = allowable shear stress.
- L_{eff} = effective mat bearing length;
- q_t = actual ground bearing pressure; and, all other terms are as previously defined.

Combining The Methods

| | | Soil Bearing Method | | | Mat Strength Method | | | Ground bearing pressure: | |
|-----------|--------------------------|---------------------------|------------|----------------------------|---------------------------|-------|-------------------------------|---------------------------|------------------------------|
| T_L | Track bearing length | 37.00 ft | | | | | | | |
| C | Bearing width of track | 5.90 ft | P | Load applied to one mat | 188,632 lbs | p | Crane load applied to one mat | 188,632 lbs | 79.15% of allowable capacity |
| T_{TL} | Track toe load | 7,993 lbs/ft ² | A_{reqd} | Required mat bearing area | 48.16 ft ² | L_c | Cantilevered length of mat | 4.66 ft | Bending stress in mat: |
| T_{HL} | Track heel load | 7,993 lbs/ft ² | L_{reqd} | Required effective length | 12.04 ft | q | GBP due to P | 3,100 lbs/ft ² | 99.98% of allowable capacity |
| B | Mat width | 4.0 ft | L_c | Cantilevered length of mat | 3.07 ft | M | Bending moment in the mat | 1,612,411 lb-in | Shear stress in mat: |
| W | Mat Length | 20.0 ft | q | GBP due to P | 3,917 lbs/ft ² | f_b | Bending stress due to M | 1400 lbs/in ² | 59.02% of allowable capacity |
| d | Mat thickness | 12.0 in | M | Bending moment in the mat | 885,851 lb-in | v | Shear in the mat | 45,329 lbs | |
| W | Weight of mat | 4,000 lbs | f_b | Bending stress due to M | 769 lbs/in ² | f_v | Shear stress due to V | 118 lbs/in ² | |
| q_a | Allowable GBP | 4,000 lbs/ft ² | V | Shear in the mat | 32,428 lbs | q_t | actual GBP | 3,166 lbs/ft ² | |
| F_b | Allowable bending stress | 1,400 lbs/in ² | f_v | Shear stress due to V | 84 lbs/in ² | | | | |
| F_v | Allowable shear stress | 200 lbs/in ² | q_t | Maximum GBP | 4,000 lbs/ft ² | | | | |
| L_{eff} | Assumed effective length | 15.21 ft | | | | | | | |
| | | | | | | | Pressure Beneath Mats: | | 3,166 lbs/ft ² |

Applications of Crane Mats

- Outrigger pads under outriggers
- Hardwood mats under outriggers
- Hardwood mats under crawler tracks

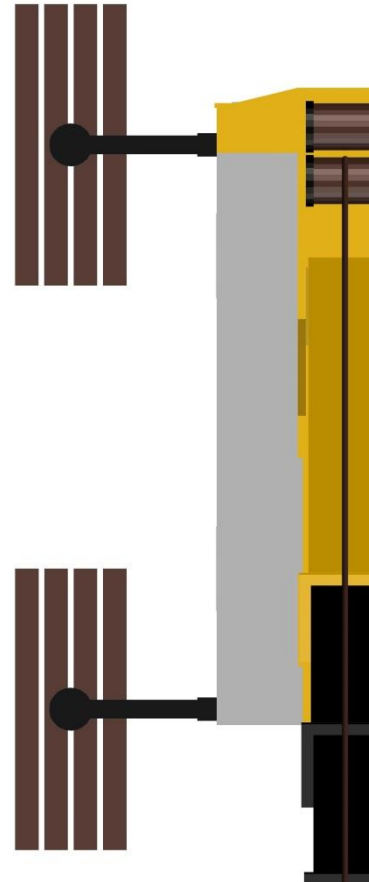
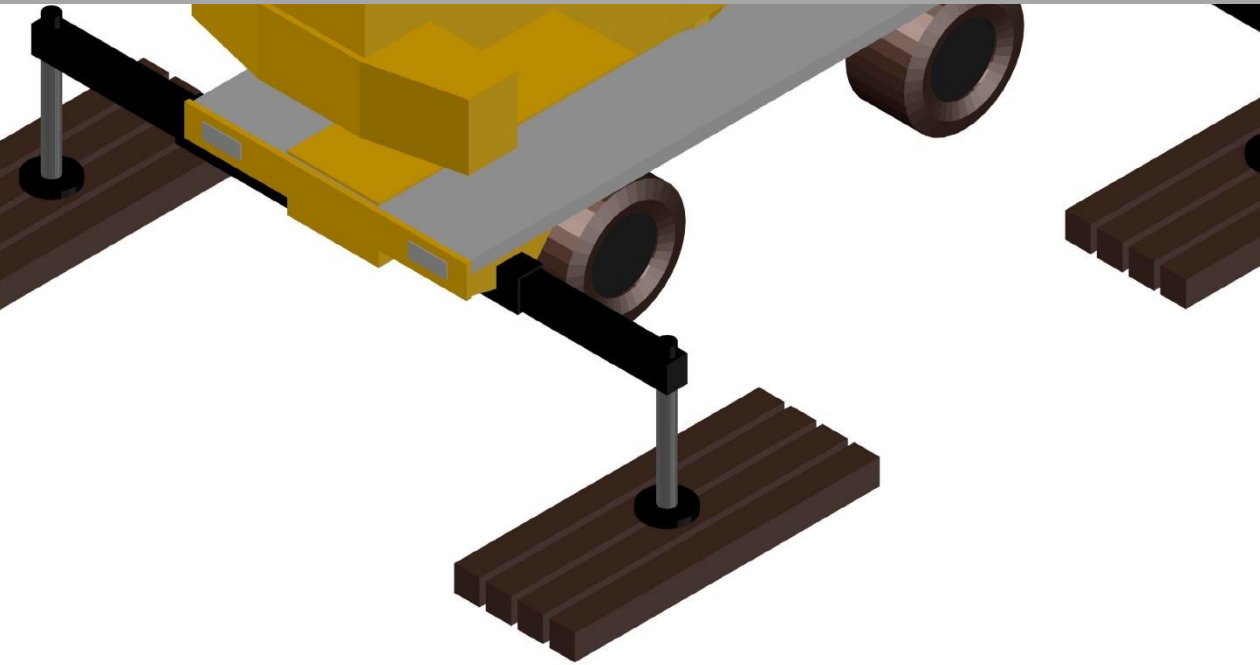
Outrigger Pads



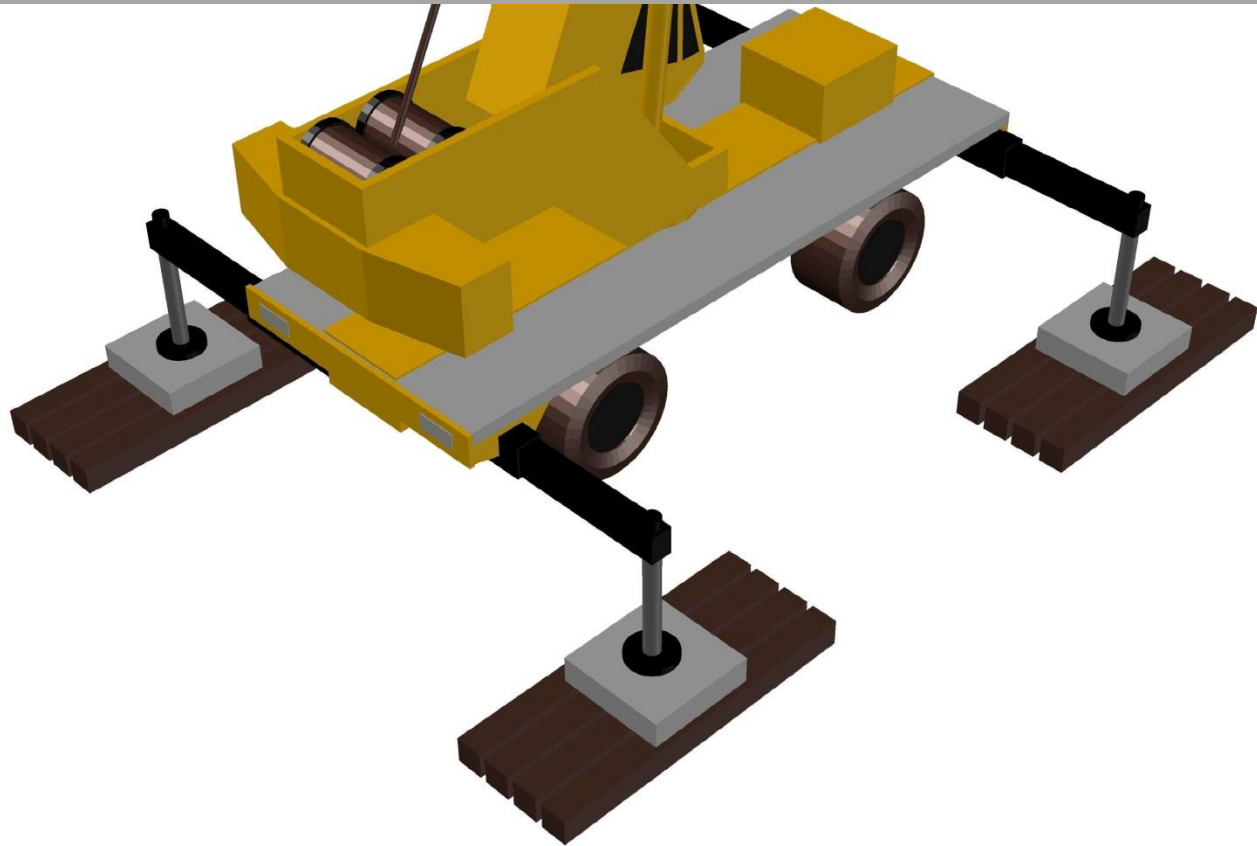
Outrigger Pad Data

| LOAD CAPACITY OF UHMW PADS (pounds) | | WIDTH | LENGTH | THICKNESS | LBS | IN ² | FT ² |
|-------------------------------------|----------|-------|--------|-----------|-----|-----------------|-----------------|
| VERTICAL | 45 ANGLE | | | | | | |
| 55,000 | 30,000 | 18" | 18" | 1" | 11 | 324 | 2.25 |
| 60,000 | 35,000 | 22" | 24" | 1" | 19 | 528 | 3.66 |
| 60,000 | 35,000 | 24" | 24" | 1" | 20 | 576 | 4 |
| 62,000 | 40,000 | 24" | 24" | 2" | 38 | 576 | 4 |
| 81,000 | 41,000 | 30" | 30" | 1" | 31 | 900 | 6.25 |
| 85,000 | 43,000 | 30" | 30" | 2" | 62 | 900 | 6.25 |
| 93,000 | 43,000 | 36" | 36" | 1" | 45 | 1296 | 9 |
| 98,000 | 45,000 | 36" | 36" | 2" | 90 | 1296 | 9 |
| 140,000 | 55,000 | 48" | 48" | 2" | 160 | 2034 | 14.125 |

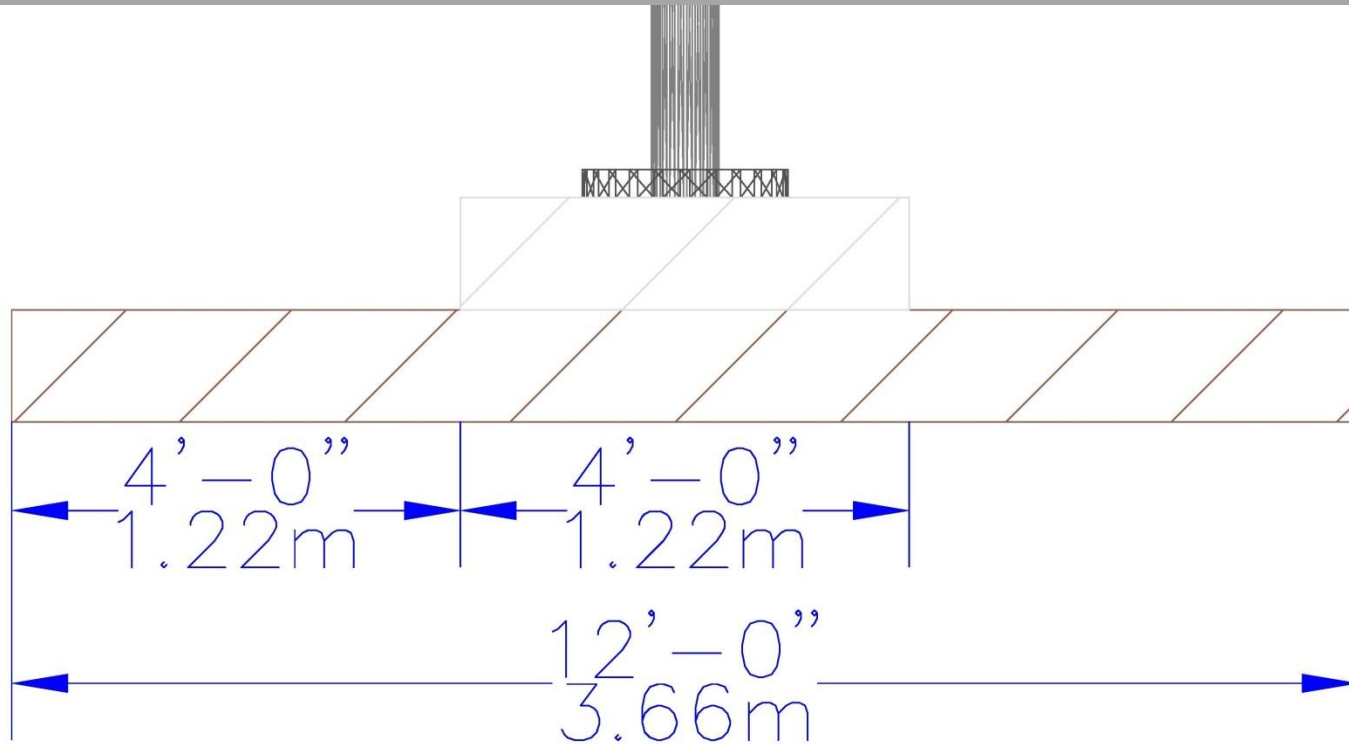
Outriggers on Crane Mats



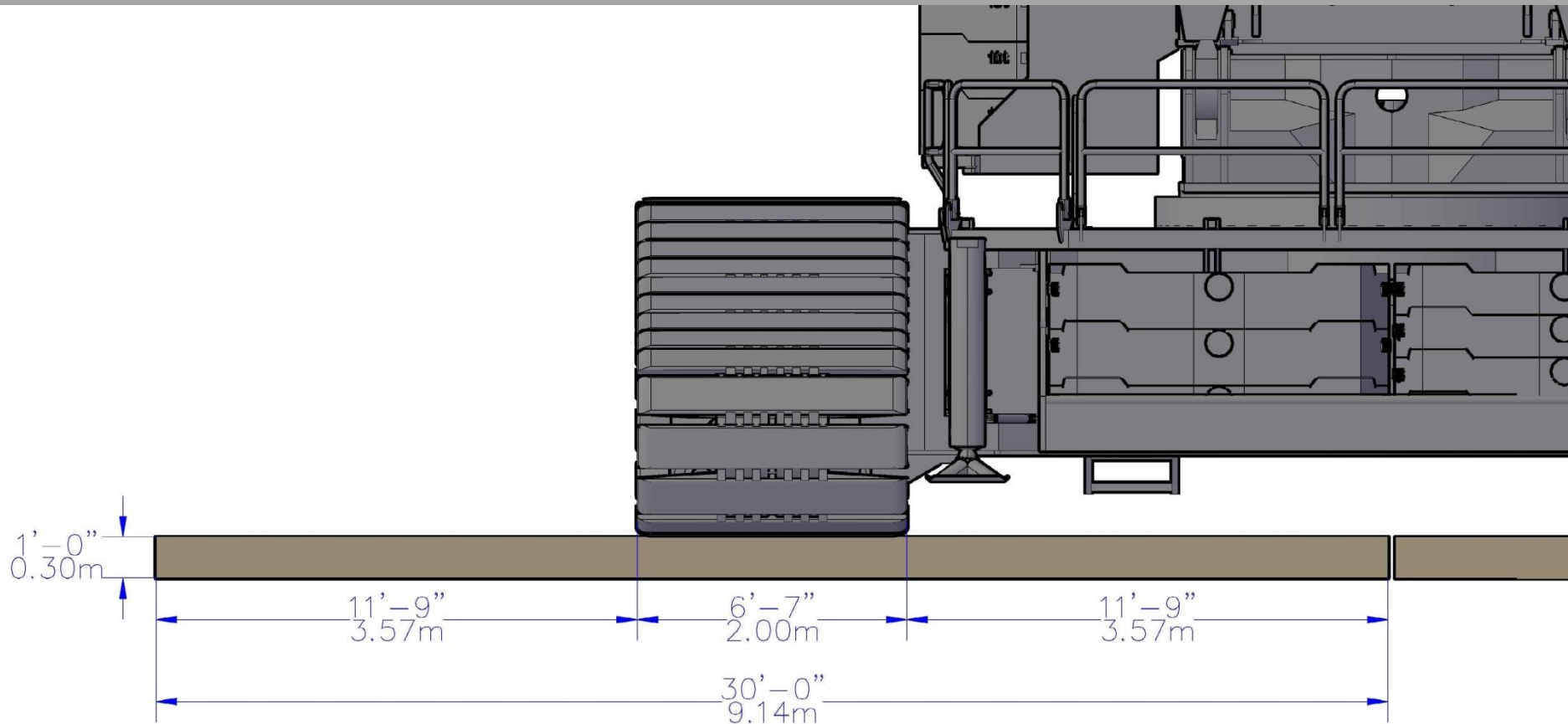
Transition Mats



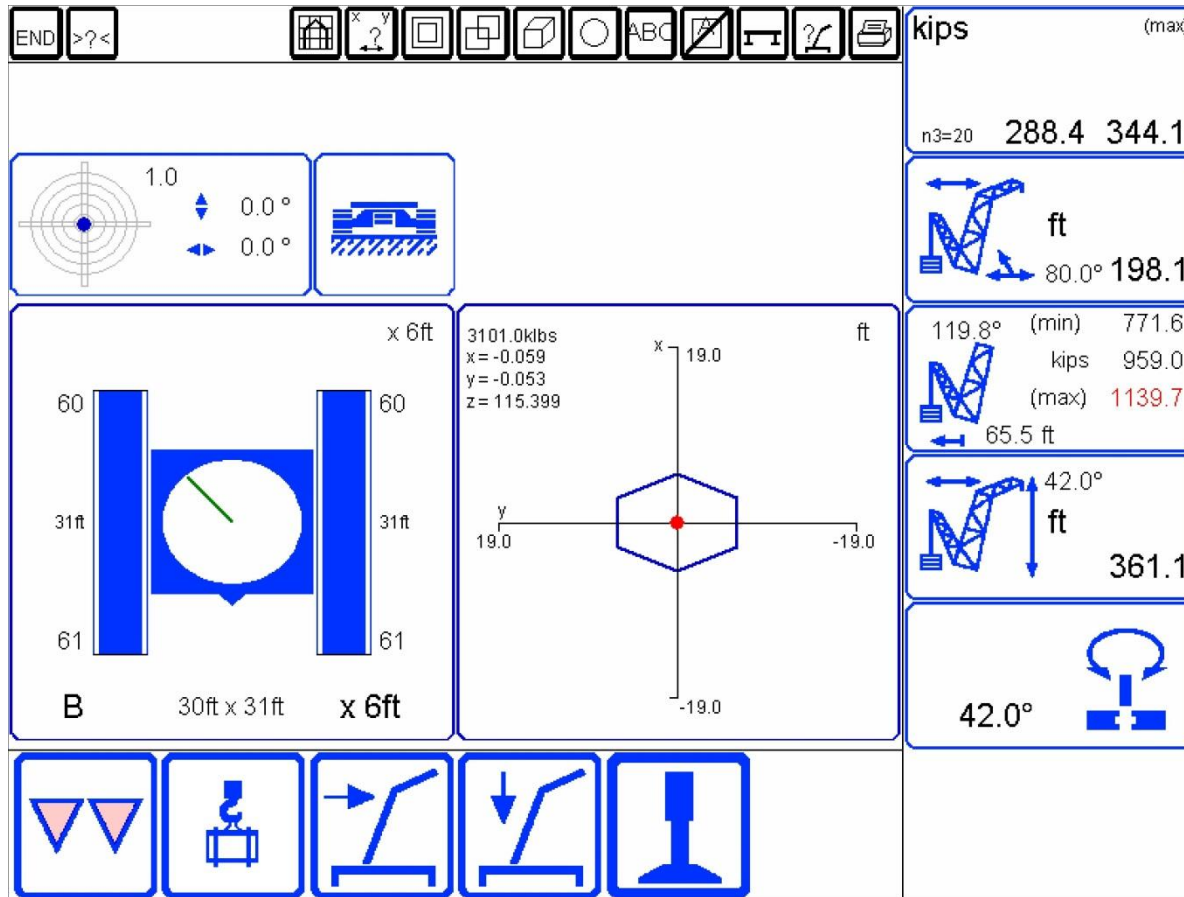
Transition Mats



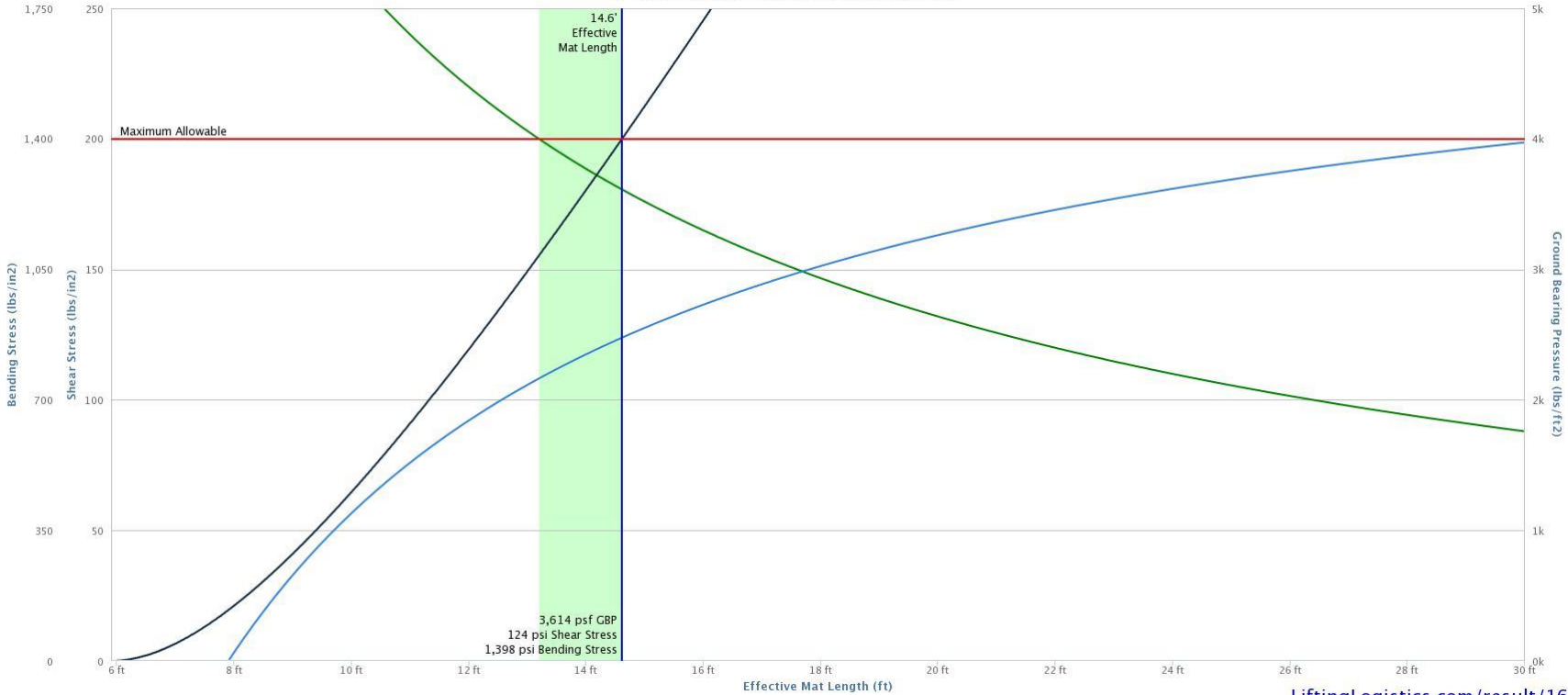
Crawlers on Mats



Crawler Example



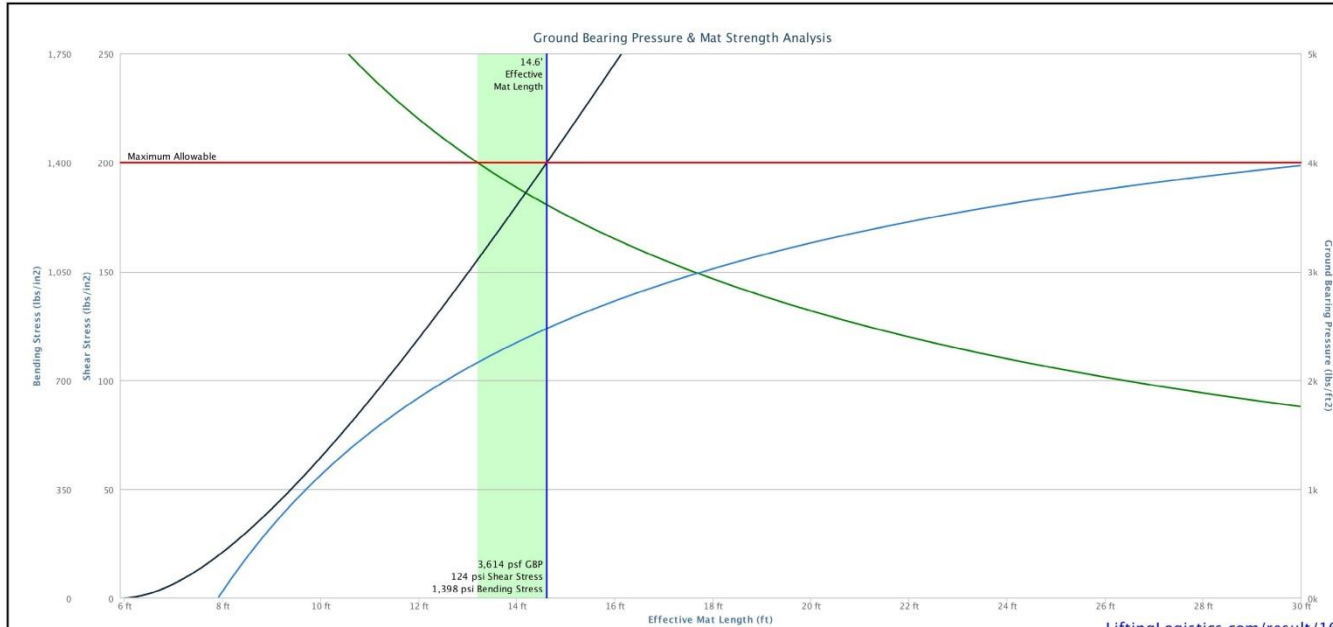
Ground Bearing Pressure & Mat Strength Analysis



LiftingLogistics.com/result/16

| T_L | Track bearing length | 31.49 ft | | Soil Bearing Method | | Mat Strength Method | | Ground bearing pressure: | |
|-----------|--------------------------|---------------------------|------------|----------------------------|---------------------------|---------------------|-------------------------------|---------------------------|------------------------------|
| C | Bearing width of track | 5.90 ft | P | Load applied to one mat | 207,087 lbs | p | Crane load applied to one mat | 207,087 lbs | 99.95% of allowable capacity |
| T_{TL} | Track toe load | 8,784 lbs/ft ² | A_{reqd} | Required mat bearing area | 52.77 ft ² | L_c | Cantilevered length of mat | 3.65 ft | Bending stress in mat: |
| T_{HL} | Track heel load | 8,640 lbs/ft ² | L_{reqd} | Required effective length | 13.19 ft | q | GBP due to P | 3,922 lbs/ft ² | 77.76% of allowable capacity |
| B | Mat width | 4.0 ft | L_c | Cantilevered length of mat | 3.65 ft | M | Bending moment in the mat | 1,254,050 lb-in | Shear stress in mat: |
| W | Mat Length | 30.0 ft | q | GBP due to P | 3,924 lbs/ft ² | f_b | Bending stress due to M | 1,089 lbs/in ² | 54.13% of allowable capacity |
| d | Mat thickness | 12.0 in | M | Bending moment in the mat | 1,252,288 lb-in | V | Shear in the mat | 41,574 lbs | |
| W | Weight of mat | 4,000 lbs | f_b | Bending stress due to M | 1,087 lbs/in ² | f_v | Shear stress due to V | 108 lbs/in ² | |
| q_a | Allowable GBP | 4,000 lbs/ft ² | V | Shear in the mat | 41,541 lbs | q_t | actual GBP | 3,998 lbs/ft ² | |
| F_b | Allowable bending stress | 1,400 lbs/in ² | f_v | Shear stress due to V | 108 lbs/in ² | | | | |
| F_v | Allowable shear stress | 200 lbs/in ² | q_t | Maximum GBP | 4,000 lbs/ft ² | | | | |
| L_{eff} | Assumed effective length | 13.20 ft | | | | | | | |
| | | | | | | | | Pressure Beneath Mats: | 3,998 lbs/ft ² |

The Actual Report



LiftingLogistics.com/result/16

PROJECT: Example Project

LOCATION: Graham, North Carolina

BUCKNER CONTACT: Keith Rind
 KeithR@bucknercompanies.com

LIFT PLAN BY: Jim Jotho
 Jjtho@bucknercompanies.com

DRAWING NOTES: Content

FILE: C:\Users\jjotho\BUCKNER\Desktop\GBP.dwg

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Revisions

All Sheets Same Revision Level

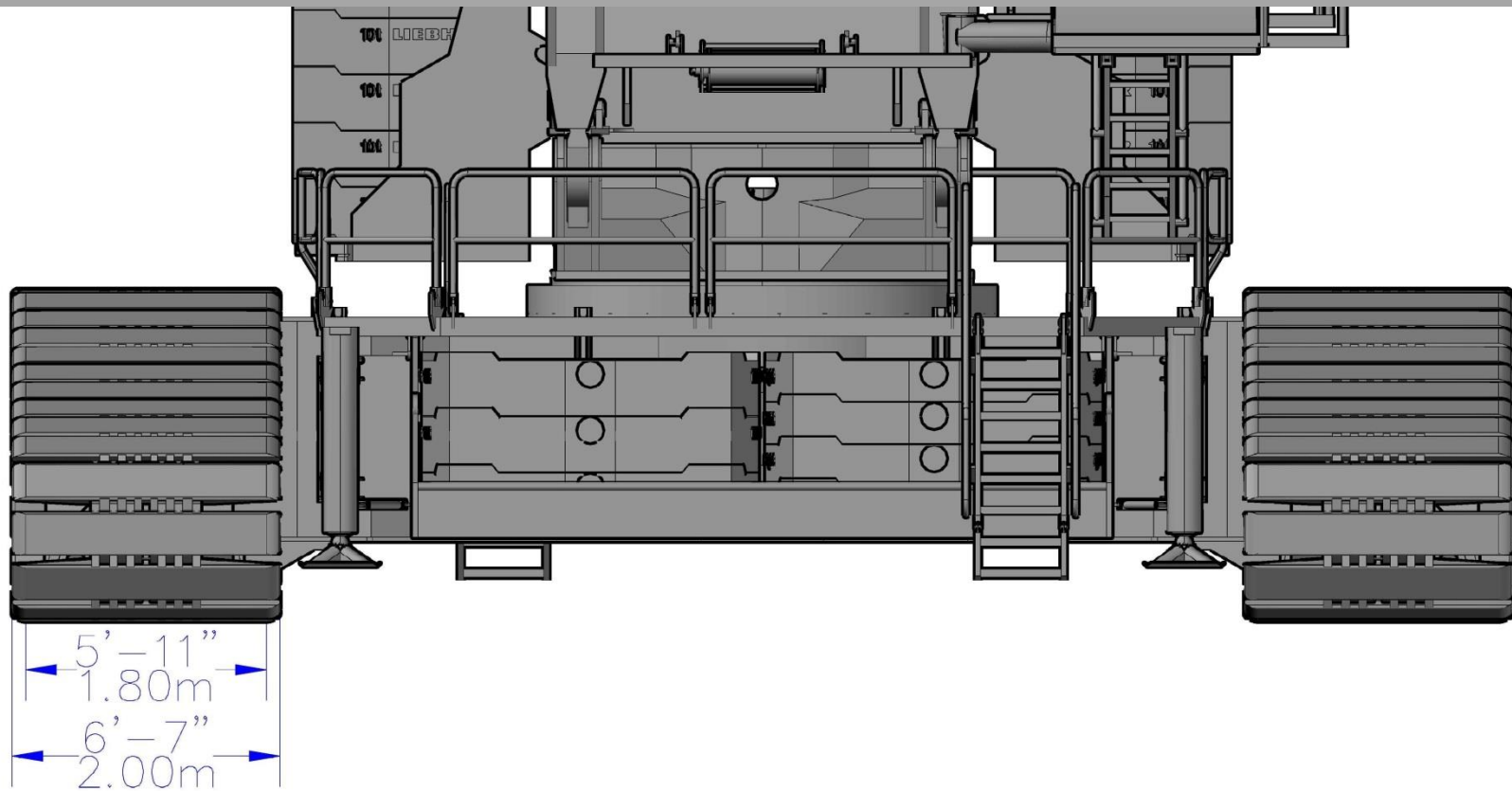
| Rev. | Date | Description |
|------|------------|---------------------------------------|
| 000 | 02.20.2013 | Preliminary Planning & Initial Layout |
| 001 | ---- | ---- |
| 002 | ---- | ---- |
| 003 | ---- | ---- |
| 004 | ---- | ---- |
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| 006 | ---- | ---- |
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SHEET: 001 OF 001

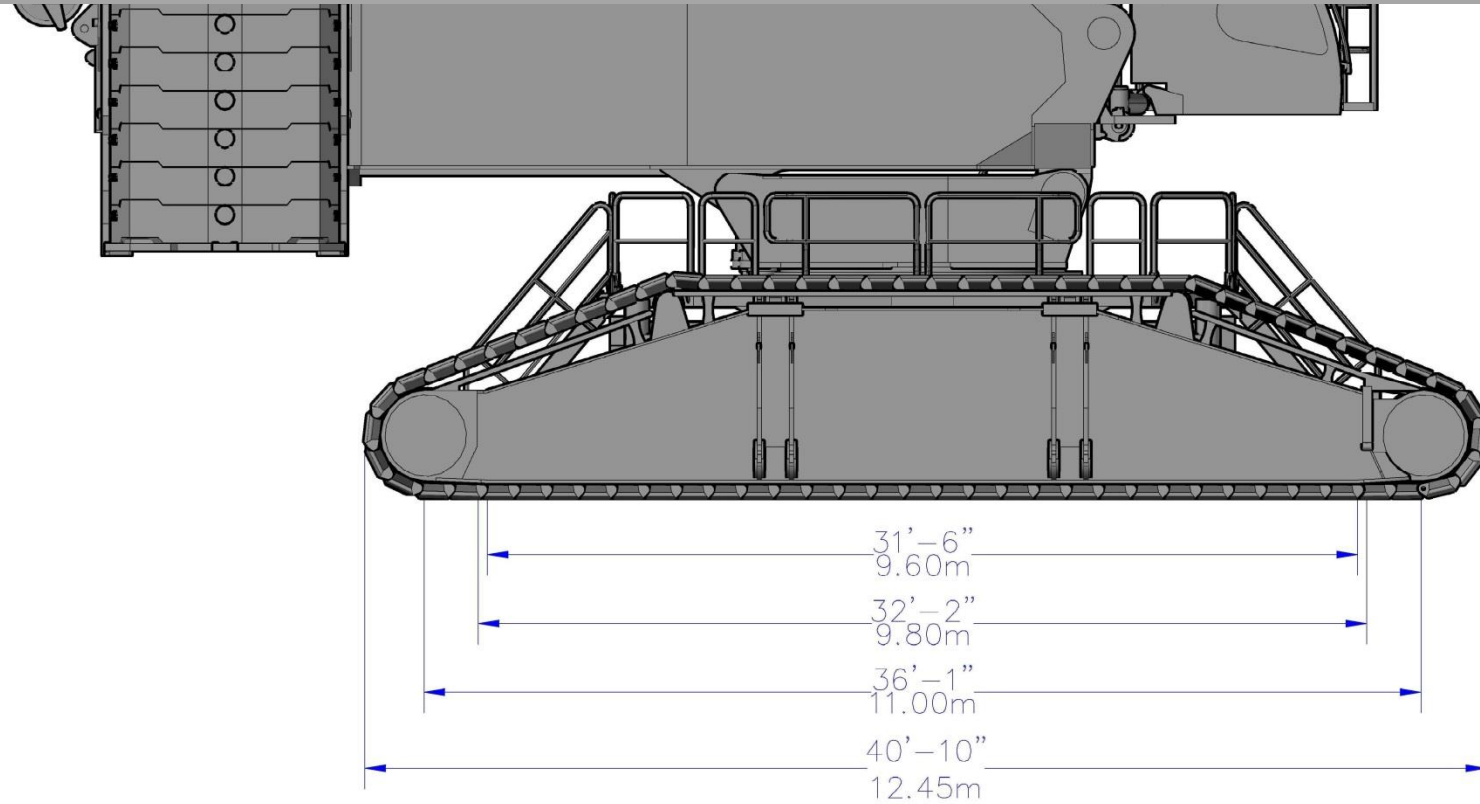
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| Track bearing length | | Soil Bearing Method | | Mat Strength Method | | Ground bearing pressure: | | | |
|-------------------------------|--------------------------|---------------------------|-------------------|----------------------------|---------------------------|--------------------------|-------------------------------|---------------------------------|------------------------------|
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| d | Mat Length | 30.0 ft | q | GBP due to P | 3,924 lbs/ft ² | f _b | Bending stress due to M | 1089 lbs/in ² | 54.13% of allowable capacity |
| W | Mat thickness | 12.0 in | M | Bending moment in the mat | 1,252,288 lb-in | V | Shear in the mat | 41,574 lbs | |
| W | Weight of mat | 4,000 lbs | f _b | Bending stress due to M | 1,087 lbs/in ² | f _v | Shear stress due to V | 108 lbs/in ² | |
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| F _v | Allowable shear stress | 200 lbs/in ² | q _t | Maximum GBP | 4,000 lbs/ft ² | | | | |
| L _{eff} | Assumed effective length | 13.20 ft | | | | | | | |
| Pressure Beneath Mats: | | | | | | | | 3,998 lbs/ft² | |

Hard vs. Soft Ground



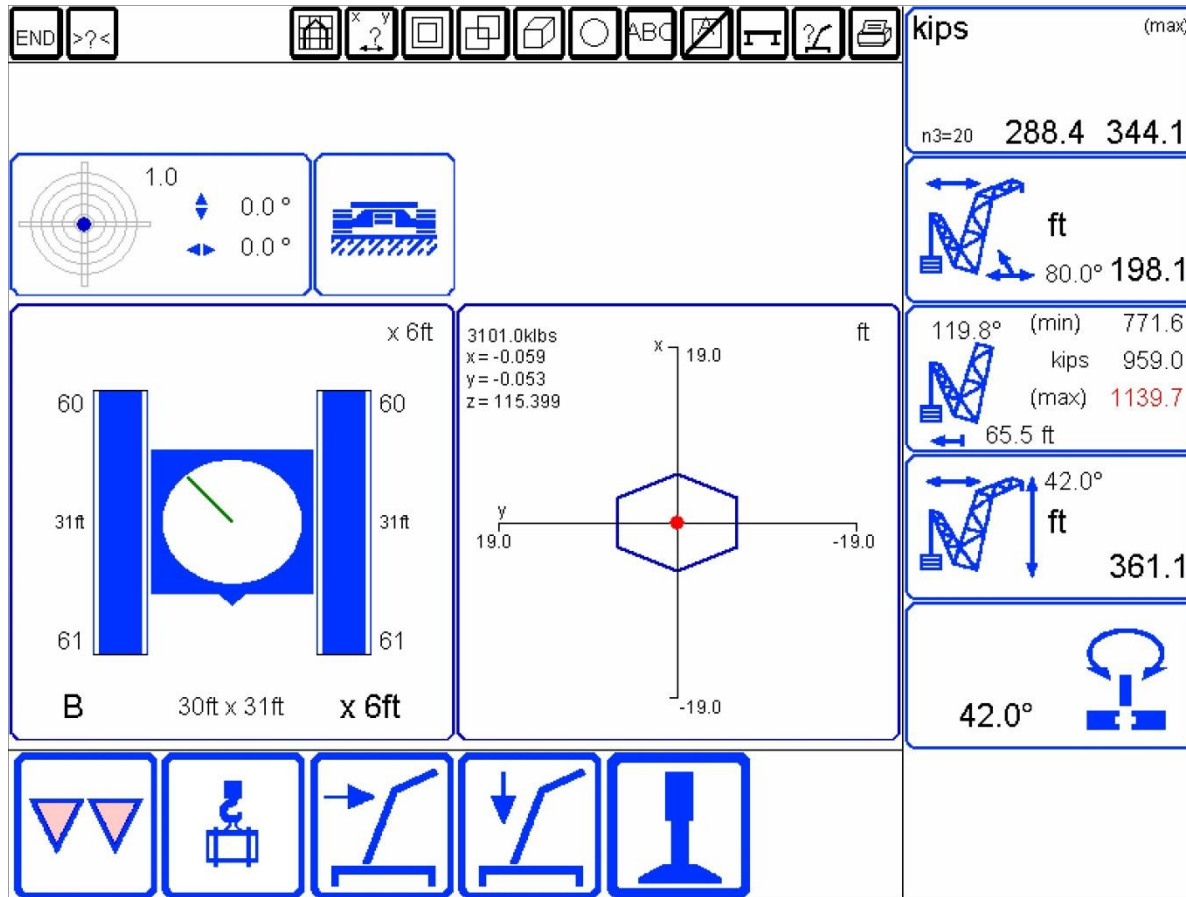
Hard vs. Soft Ground



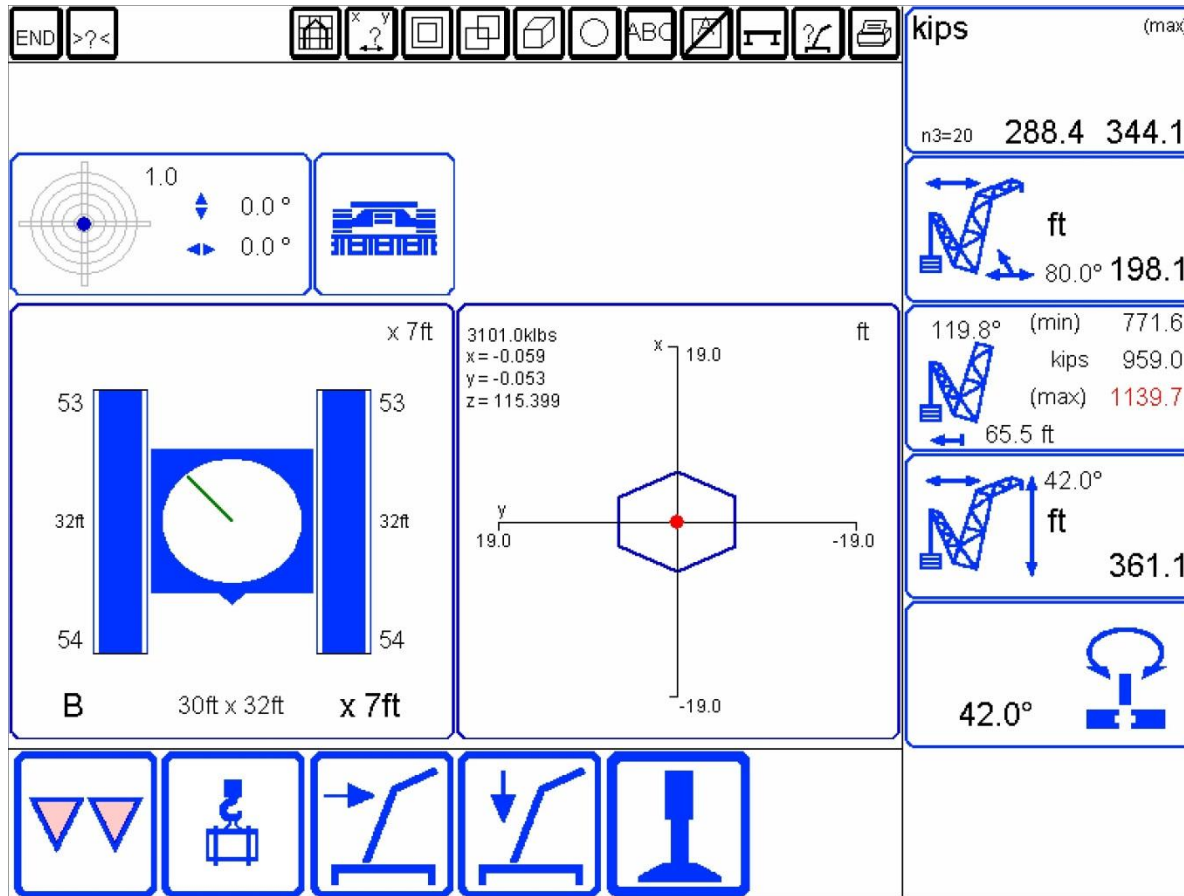
Hard vs. Soft Ground

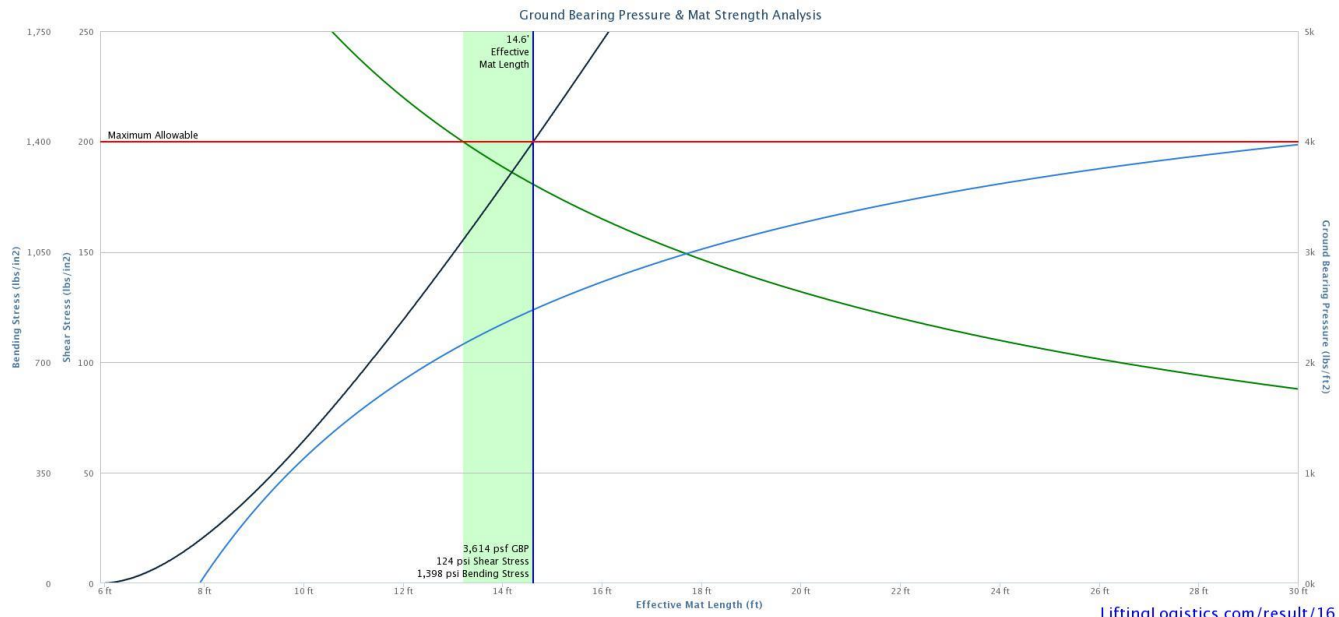
| | Soft Ground | | | Hard Ground | | | % Difference in bearing area |
|----------|-------------|------------|-------------------------|-------------|------------|-------------------------|------------------------------|
| | Length (in) | Width (in) | Area (in ²) | Length (in) | Width (in) | Area (in ²) | |
| 777 | 257.5 | 47.3 | 12179.75 | 209 | 20.3 | 4242.7 | 287% |
| 888 | 296 | 47.3 | 14000.8 | 240 | 20.3 | 4872 | 287% |
| 999 | 296 | 47.3 | 14000.8 | 240 | 20.3 | 4872 | 287% |
| 16000 | 355 | 60 | 21300 | 296.5 | 50 | 14825 | 144% |
| 18000 | 414.5 | 60 | 24870 | 348 | 50 | 17400 | 143% |
| LR 11000 | 385.82 | 78.74 | 30379.47 | 377.95 | 70.86 | 26781.54 | 113% |

Hard Ground Numbers

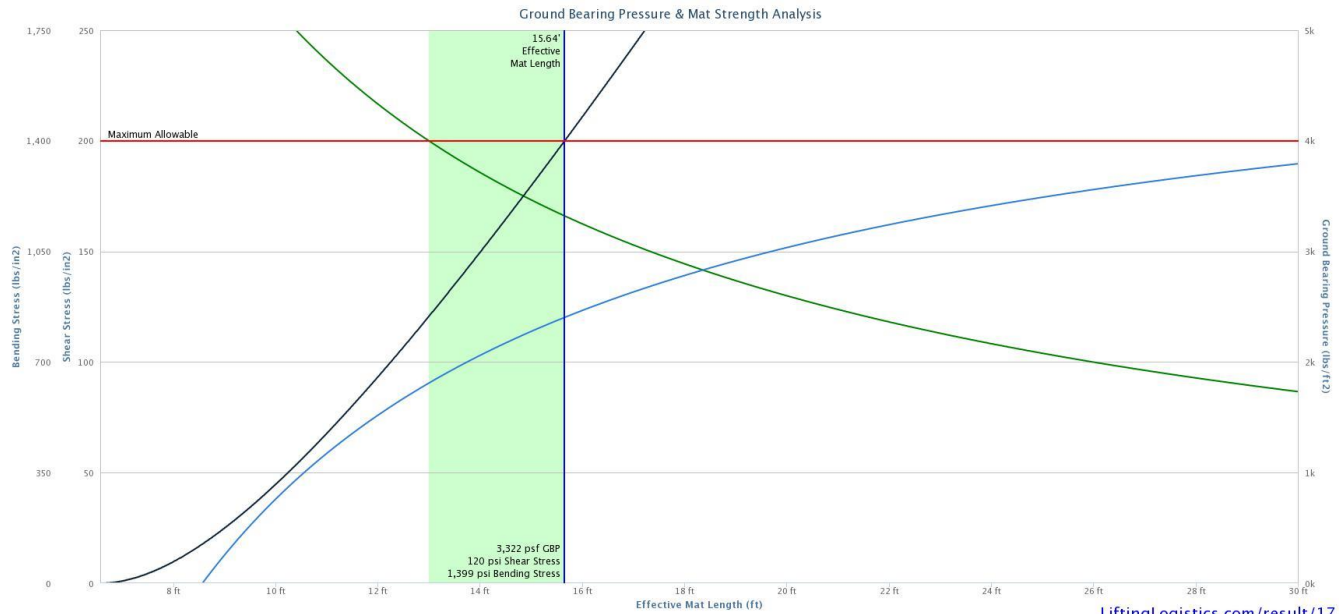


Soft Ground Numbers





LiftingLogistics.com/result/16



LiftingLogistics.com/result/17

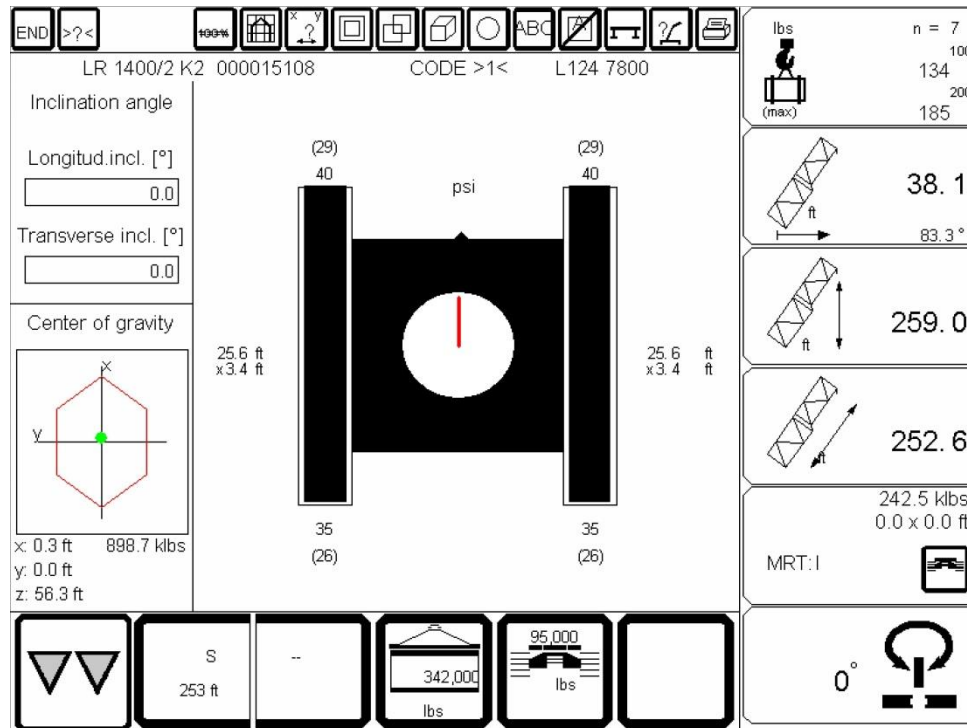
Hard vs. Soft Tables

| T _L | Track bearing length | 31.49 ft | | Soil Bearing Method | | | Mat Strength Method | | | Ground bearing pressure: |
|------------------|--------------------------|---------------------------|-------------------|----------------------------|---------------------------|----------------|-------------------------------|---------------------------|------------------------|------------------------------|
| C | Bearing width of track | 5.90 ft | P | Load applied to one mat | 207,087 lbs | p | Crane load applied to one mat | 207,087 lbs | | 90.36% of allowable capacity |
| T _{TL} | Track toe load | 8,784 lbs/ft ² | A _{reqd} | Required mat bearing area | 52.77 ft ² | L _c | Cantilevered length of mat | 4.35 ft | | Bending stress in mat: |
| T _{HL} | Track heel load | 8,640 lbs/ft ² | L _{reqd} | Required effective length | 13.19 ft | q | GBP due to P | 3,546 lbs/ft ² | | 99.85% of allowable capacity |
| B | Mat width | 4.0 ft | L _c | Cantilevered length of mat | 3.65 ft | M | Bending moment in the mat | 1,610,382 lb-in | | Shear stress in mat: |
| W | Mat Length | 30.0 ft | q | GBP due to P | 3,924 lbs/ft ² | f _b | Bending stress due to M | 1398 lbs/in ² | | 61.87% of allowable capacity |
| d | Mat thickness | 12.0 in | M | Bending moment in the mat | 1,252,288 lb-in | V | Shear in the mat | 47,516 lbs | | |
| W | Weight of mat | 4,000 lbs | f _b | Bending stress due to M | 1,087 lbs/in ² | f _v | Shear stress due to V | 124 lbs/in ² | | |
| q _a | Allowable GBP | 4,000 lbs/ft ² | V | Shear in the mat | 41,541 lbs | q _t | actual GBP | 3,614 lbs/ft ² | | |
| F _b | Allowable bending stress | 1,400 lbs/in ² | f _v | Shear stress due to V | 108 lbs/in ² | | | | | |
| F _v | Allowable shear stress | 200 lbs/in ² | q _t | Maximum GBP | 4,000 lbs/ft ² | | | | | |
| L _{eff} | Assumed effective length | 14.60 ft | | | | | | | | |
| | | | | | | | | | Pressure Beneath Mats: | 3,614 lbs/ft ² |

| T _L | Track bearing length | 32.15 ft | | Soil Bearing Method | | | Mat Strength Method | | | Ground bearing pressure: |
|------------------|--------------------------|---------------------------|-------------------|----------------------------|---------------------------|----------------|-------------------------------|---------------------------|------------------------|------------------------------|
| C | Bearing width of track | 6.56 ft | P | Load applied to one mat | 203,807 lbs | p | Crane load applied to one mat | 203,807 lbs | | 83.04% of allowable capacity |
| T _{TL} | Track toe load | 7,776 lbs/ft ² | A _{reqd} | Required mat bearing area | 51.95 ft ² | L _c | Cantilevered length of mat | 4.54 ft | | Bending stress in mat: |
| T _{HL} | Track heel load | 7,632 lbs/ft ² | L _{reqd} | Required effective length | 12.99 ft | q | GBP due to P | 3,258 lbs/ft ² | | 99.92% of allowable capacity |
| B | Mat width | 4.0 ft | L _c | Cantilevered length of mat | 3.21 ft | M | Bending moment in the mat | 1,611,557 lb-in | | Shear stress in mat: |
| W | Mat Length | 30.0 ft | q | GBP due to P | 3,923 lbs/ft ² | f _b | Bending stress due to M | 1399 lbs/in ² | | 60.07% of allowable capacity |
| d | Mat thickness | 12.0 in | M | Bending moment in the mat | 972,557 lb-in | V | Shear in the mat | 46,130 lbs | | |
| W | Weight of mat | 4,000 lbs | f _b | Bending stress due to M | 844 lbs/in ² | f _v | Shear stress due to V | 120 lbs/in ² | | |
| q _a | Allowable GBP | 4,000 lbs/ft ² | V | Shear in the mat | 34,742 lbs | q _t | actual GBP | 3,322 lbs/ft ² | | |
| F _b | Allowable bending stress | 1,400 lbs/in ² | f _v | Shear stress due to V | 90 lbs/in ² | | | | | |
| F _v | Allowable shear stress | 200 lbs/in ² | q _t | Maximum GBP | 4,000 lbs/ft ² | | | | | |
| L _{eff} | Assumed effective length | 15.64 ft | | | | | | | | |
| | | | | | | | | | Pressure Beneath Mats: | 3,322 lbs/ft ² |

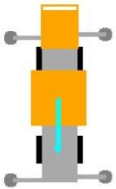
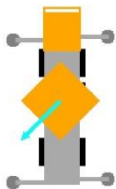

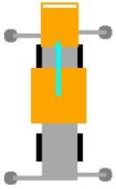



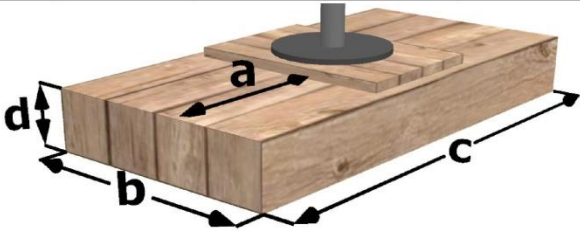
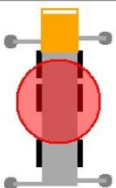


Liebherr – Hard vs. Soft?

LR 1400, LR 1600, and LR 1750 have no additional allowance for bearing area in Liccon



Load Case Scenarios

Ground Bearing Pressure – Grove GMK 7550, Maximum Radius, Fully Loaded.

| Directly Over Rear of Crane | | Over Aft Left Outrigger | | Directly Over Left Side | | Over Front Left Outrigger | | | | |
|---|--|---|---------------------------|---|----------------------------|---|----------------------------|---------------------------|---|----------------------------|
| Front Left: 95,591lbs |  | Front Right: 95,591lbs | Front Left: 165,143lbs |  | Front Right: 71,204lbs | Front Left: 239,217lbs | Front Right: 106,339lbs | Front Left: 274,439lbs |  | Front Right: 180,413lbs |
| Aft Left: 259,409lbs | | Aft Right: 259,409lbs | Aft Left: 297,348lbs | | Aft Right: 176,291lbs | Aft Left: 267,735lbs | Aft Right: 96,609lbs | Aft Left: 188,052lbs | | Aft Right: 67,096lbs |
| Directly Over Front of Crane | | Over Front Right Outrigger | | Directly Over Right Side | | Over Aft Right Outrigger | | | | |
| Front Left: 250,052lbs |  | Front Right: 250,052lbs | Front Left: 180,413lbs |  | Front Right: 274,439lbs | Front Left: 106,339lbs | Front Right: 239,217lbs | Front Left: 71,204lbs |  | Front Right: 165,143lbs |
| Aft Left: 104,948lbs | | Aft Right: 104,948lbs | Aft Left: 67,096lbs | | Aft Right: 188,052lbs | Aft Left: 96,609lbs | Aft Right: 267,735lbs | Aft Left: 176,291lbs | | Aft Right: 297,348lbs |
| Full 360 Degree Rotation | | Mat Configuration: Three 4' x 12' by 1' mats side by side under a 10' x 8' x 11" steel transition mat per outrigger. | |  | |  | | | | |
| Front Left: 274,439lbs |  | Front Right: 274,439lbs | | | | | | | | |
| Aft Left: 297,348lbs | | Aft Right: 297,348lbs | | | | | | | | |
| Crane Configuration: Boom Length: 125.1' main boom, MegaWingLift Counterweight: 352,700lbs Support Base: 28'9" by 29'2" Load Radius: Maximum of 60ft Load Weight: 140,000lbs | | | |  | |  | | | | |

Printed Large Dataset



| Contents | | | | | |
|----------|---|-------|--|-------|--|
| Sheet | Description | Sheet | Description | Sheet | Description |
| 001 | Title Page | 031 | 253' S Boom 37737lbs Load Min Radius GBP | 061 | 253' S Boom 128363lbs Load Max Radius GBP |
| 002 | Summary | 032 | 253' S Boom 37737lbs Load Max Radius Liccon | 062 | 253'+57' S2F2 0lbs Load Min Radius Liccon |
| 003 | 253' S Boom Load Chart | 033 | 253' S Boom 37737lbs Load Max Radius GBP | 063 | 253'+57' S2F2 0lbs Load Min Radius GBP |
| 004 | 253'-57' S2F2 Load Chart | 034 | 253' S Boom 43670lbs Load Min Radius Liccon | 064 | 253'+57' S2F2 0lbs Load Max Radius Liccon |
| 005 | Block Weight | 035 | 253' S Boom 43670lbs Load Min Radius GBP | 065 | 253'+57' S2F2 0lbs Load Max Radius GBP |
| 006 | 253' S Boom 0lbs Load Min Radius Liccon | 036 | 253' S Boom 43670lbs Load Max Radius Liccon | 066 | 253'+57' S2F2 63641lbs Load Min Radius Liccon |
| 007 | 253' S Boom 0lbs Load Min Radius GBP | 037 | 253' S Boom 43670lbs Load Max Radius GBP | 067 | 253'+57' S2F2 63641lbs Load Min Radius GBP |
| 008 | 253' S Boom 0lbs Load Max Radius Liccon | 038 | 253' S Boom 50791lbs Load Min Radius Liccon | 068 | 253'+57' S2F2 63641lbs Load Max Radius Liccon |
| 009 | 253' S Boom 0lbs Load Max Radius GBP | 039 | 253' S Boom 50791lbs Load Min Radius GBP | 069 | 253'+57' S2F2 63641lbs Load Max Radius GBP |
| 010 | 253' S Boom 5601lbs Load Min Radius Liccon | 040 | 253' S Boom 50791lbs Load Max Radius Liccon | 070 | 253'+57' S2F2 78582lbs Load Min Radius Liccon |
| 011 | 253' S Boom 5601lbs Load Min Radius GBP | 041 | 253' S Boom 50791lbs Load Max Radius GBP | 071 | 253'+57' S2F2 78582lbs Load Min Radius GBP |
| 012 | 253' S Boom 5601lbs Load Max Radius Liccon | 042 | 253' S Boom 52113lbs Load Min Radius Liccon | 072 | 253'+57' S2F2 78582lbs Load Max Radius Liccon |
| 013 | 253' S Boom 5601lbs Load Max Radius GBP | 043 | 253' S Boom 52113lbs Load Min Radius GBP | 073 | 253'+57' S2F2 78582lbs Load Max Radius GBP |
| 014 | 253' S Boom 8134lbs Load Min Radius Liccon | 044 | 253' S Boom 52113lbs Load Max Radius Liccon | 074 | 253'+57' S2F2 81719lbs Load Min Radius Liccon |
| 015 | 253' S Boom 8134lbs Load Min Radius GBP | 045 | 253' S Boom 52113lbs Load Max Radius GBP | 075 | 253'+57' S2F2 81719lbs Load Min Radius GBP |
| 016 | 253' S Boom 8134lbs Load Max Radius Liccon | 046 | 253' S Boom 59830lbs Load Min Radius Liccon | 076 | 253'+57' S2F2 81719lbs Load Max Radius Liccon |
| 017 | 253' S Boom 8134lbs Load Max Radius GBP | 047 | 253' S Boom 59830lbs Load Min Radius GBP | 077 | 253'+57' S2F2 81719lbs Load Max Radius GBP |
| 018 | 253' S Boom 13664lbs Load Min Radius Liccon | 048 | 253' S Boom 59830lbs Load Max Radius Liccon | 078 | 253'+57' S2F2 112363lbs Load Min Radius Liccon |
| 019 | 253' S Boom 13664lbs Load Min Radius GBP | 049 | 253' S Boom 59830lbs Load Max Radius GBP | 079 | 253'+57' S2F2 112363lbs Load Min Radius GBP |
| 020 | 253' S Boom 13664lbs Load Max Radius Liccon | 050 | 253' S Boom 81719lbs Load Min Radius Liccon | 080 | 253'+57' S2F2 112363lbs Load Max Radius Liccon |
| 021 | 253' S Boom 13664lbs Load Max Radius GBP | 051 | 253' S Boom 81719lbs Load Min Radius GBP | 081 | 253'+57' S2F2 112363lbs Load Max Radius GBP |
| 022 | 253' S Boom 30541lbs Load Min Radius Liccon | 052 | 253' S Boom 81719lbs Load Max Radius Liccon | 082 | 253'+57' S2F2 128363lbs Load Min Radius Liccon |
| 023 | 253' S Boom 30541lbs Load Min Radius GBP | 053 | 253' S Boom 81719lbs Load Max Radius GBP | 083 | 253'+57' S2F2 128363lbs Load Min Radius GBP |
| 024 | 253' S Boom 30541lbs Load Max Radius Liccon | 054 | 253' S Boom 112363lbs Load Min Radius Liccon | 084 | 253'+57' S2F2 128363lbs Load Max Radius Liccon |
| 025 | 253' S Boom 30541lbs Load Max Radius GBP | 055 | 253' S Boom 112363lbs Load Min Radius GBP | 085 | 253'+57' S2F2 128363lbs Load Max Radius GBP |
| 026 | 253' S Boom 32791lbs Load Min Radius Liccon | 056 | 253' S Boom 112363lbs Load Max Radius Liccon | | |
| 027 | 253' S Boom 32791lbs Load Min Radius GBP | 057 | 253' S Boom 112363lbs Load Max Radius GBP | | |
| 028 | 253' S Boom 32791lbs Load Max Radius Liccon | 058 | 253' S Boom 128363lbs Load Min Radius Liccon | | |
| 029 | 253' S Boom 32791lbs Load Max Radius GBP | 059 | 253' S Boom 128363lbs Load Min Radius GBP | | |
| 030 | 253' S Boom 37737lbs Load Min Radius Liccon | 060 | 253' S Boom 128363lbs Load Max Radius Liccon | | |

PROJECT: [REDACTED]

LOCATION: [REDACTED]

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LIFT PLAN BY: Jim Jetho
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DRAWING NOTES:
Title Page

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| 002 | ---- | ---- |
| 003 | ---- | ---- |
| 004 | ---- | ---- |
| 005 | ---- | ---- |
| 006 | ---- | ---- |
| 007 | ---- | ---- |
| 008 | ---- | ---- |
| 009 | ---- | ---- |
| 010 | ---- | ---- |

SHEET: 001 OF 085

BUCKNER
HEAVYLIFT CRANES

Printed Large Dataset

PROJECT: [REDACTED]

LOCATION: [REDACTED]

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LIFT PLAN BY: Jim Jetho
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| 000 | 02.17.2014 | Preliminary Planning & Initial Layout |
| 001 | ---- | ---- |
| 002 | ---- | ---- |
| 003 | ---- | ---- |
| 004 | ---- | ---- |
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| 010 | ---- | ---- |

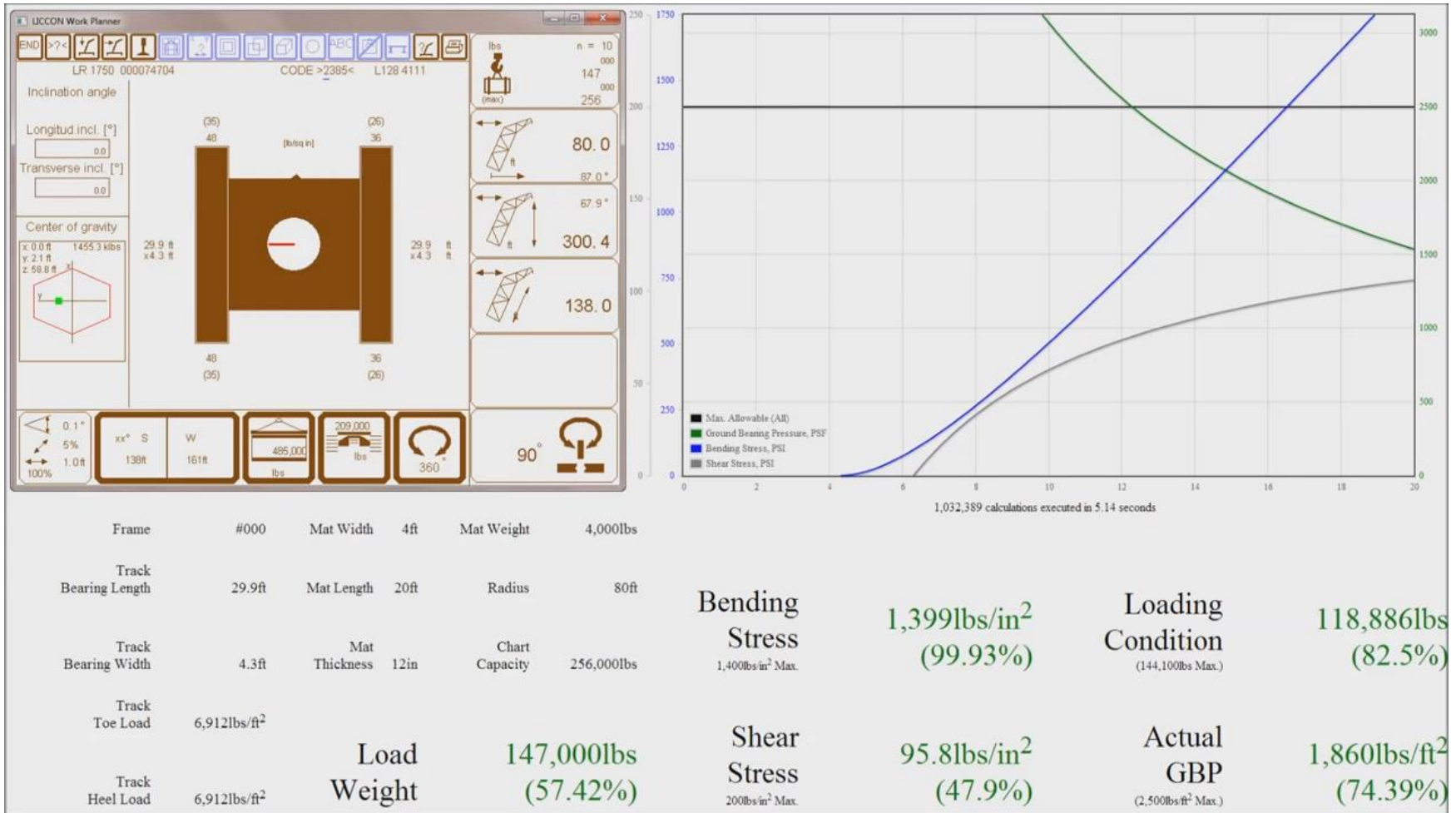
SHEET: 002 OF 085

BUCKNER
HEAVYLIFT CRANES

Ground Bearing Pressure Summary

| Load Case | Minimum Radius | GBP At Minimum Radius | Maximum Radius | GBP At Maximum Radius |
|-------------------------------|----------------|--------------------------|----------------|--------------------------|
| 253' S 0lbs Load | 38'-1" | 2,729lbs/ft ² | 230'-0" | 3,544lbs/ft ² |
| 253' S 5,601lbs Load | 38'-1" | 2,594lbs/ft ² | 213'-9" | 3,982lbs/ft ² |
| 253' S 8,134lbs Load | 38'-1" | 2,548lbs/ft ² | 204'-8" | 3,985lbs/ft ² |
| 253' S 13,864lbs Load | 38'-1" | 2,410lbs/ft ² | 187'-9" | 3,992lbs/ft ² |
| 253' S 30,541lbs Load | 38'-1" | 2,142lbs/ft ² | 149'-8" | 3,963lbs/ft ² |
| 253' S 32,791lbs Load | 38'-1" | 2,095lbs/ft ² | 145'-8" | 3,967lbs/ft ² |
| 253' S 37,737lbs Load | 38'-1" | 2,005lbs/ft ² | 137'-10" | 3,974lbs/ft ² |
| 253' S 43,670lbs Load | 38'-1" | 1,975lbs/ft ² | 129'-7" | 3,984lbs/ft ² |
| 253' S 50,791lbs Load | 38'-1" | 1,835lbs/ft ² | 121'-0" | 3,984lbs/ft ² |
| 253' S 52,113lbs Load | 38'-1" | 1,778lbs/ft ² | 119'-6" | 3,987lbs/ft ² |
| 253' S 59,830lbs Load | 38'-1" | 1,705lbs/ft ² | 111'-6" | 3,993lbs/ft ² |
| 253' S 81,719lbs Load | 38'-1" | 1,422lbs/ft ² | 93'-2" | 3,911lbs/ft ² |
| 253' S 112,363lbs Load | 38'-1" | 1,048lbs/ft ² | 76'-6" | 3,992lbs/ft ² |
| 253' S 128,363lbs Load | 38'-1" | 1,020lbs/ft ² | 69'-3" | 3,902lbs/ft ² |
| 253'/57' S2F2 0lbs Load | 45'-6" | 2,556lbs/ft ² | 205'-4" | 3,850lbs/ft ² |
| 253'/57' S2F2 69,361lbs Load | 45'-6" | 1,385lbs/ft ² | 103'-6" | 3,967lbs/ft ² |
| 253'/57' S2F2 78,582lbs Load | 45'-6" | 1,156lbs/ft ² | 92'-7" | 3,986lbs/ft ² |
| 253'/57' S2F2 81,179lbs Load | 45'-6" | 1,081lbs/ft ² | 90'-6" | 3,931lbs/ft ² |
| 253'/57' S2F2 112,363lbs Load | 45'-6" | 1,201lbs/ft ² | 74'-9" | 3,963lbs/ft ² |
| 253'/57' S2F2 128,363lbs Load | 45'-6" | 1,526lbs/ft ² | 68'-4" | 3,918lbs/ft ² |

GBP Analysis Animation



Summary

- Are all timbers of the mat being loaded when under an outrigger?
- Is the full length of the mat being considered as “effective”?
 - If so, what are the bearing and shear stresses in the mat?
 - If not, what effective length is bearing into the soil?
- Have all worst case scenarios been considered?
 - Empty hook conditions?
 - Worst case swing angles?
 - Crane erection?
- Are hard ground or soft ground numbers being used for crawler track pressures?
 - Does the effective bearing area of the tracks match the soft/hard ground condition?
 - If soft ground numbers are being used, what is the justification?

QUESTIONS?